

## **Unintended Ignition Switch Rotation**

April 28, 2014

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Title: Key torque to turn

Project Leader: XXXX
Project Sponsor: XXXX

Project:

# XXX

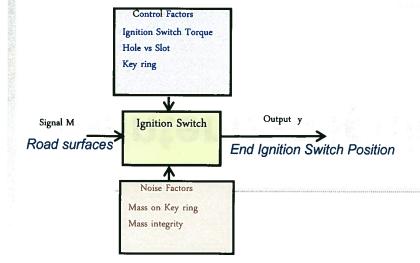
DFSS Coach:

XXXXXX

#### Project Scope

• Determine objective test that causes ignition switch to unintentionally rotate away from run towards accessory

### P-diagram



#### Findings / Learnings

- Determined 8 objective events that cause unintended key rotation
- Demonstrated proposed design performance as robust

#### Implementation

- Ensure ignition switch torque is 20N\*cm +/-5
- Further increase robustness by changing key head to design to a hole from a slot.

## 1

#### **Benefits**

• Customer has system that is very robust to unintended key rotation





## Opportunity Statement / Expected Outcome

**Opportunity Statement:** A test has not been identified that causes ignition switch to transition from 'run' to 'accessory'.

What's in it for the customer? A robust ignition switch.

What's in it for GM? A robust ignition switch.

**Expected Outcome (Specific Deliverables to the program):** A test that will establish a condition that causes the ignition switch to move from 'run' to 'accessory'. The test will be used to assess the performance of the proposed ignition switch.



## Test Procedure

Controls:

#### 18

Ignition Switch Torque to Turn Hole vs Slot on key head Key ring size / quantity

#### Signals:

Ride and Handling Loop @ Posted Speeds

Belgian Blocks Durability Schedule

Pothole #1 @ 25MPH

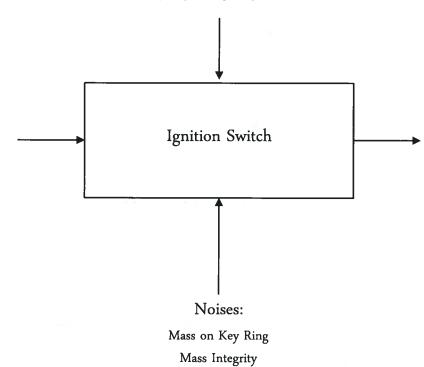
Pothole #2 @ 25MPH

Cubilete @ 10MPH

Panic Stop from 10MPH

R&H Chatter @ 45-55MPH

R&H Angled RR Crossing @ 70MPH



### Response:

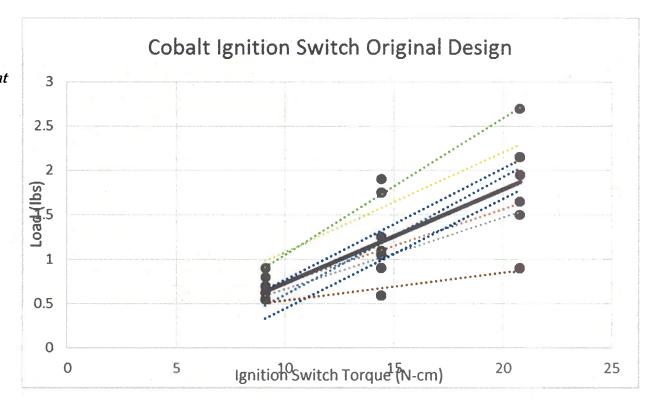
End Ignition Switch Position
- Run or Accessory

Copyright 2005 General Motors Corporation October 24, 2005 - Version 4.3



# Test Results – Original Design

Data shows that increasing switch torque, increases robustness to inertial load





Plotted the maximum load for each test signal that ended with ignition switch in 'run' position. Bold line is average of all tests. Described as maximum load success line.

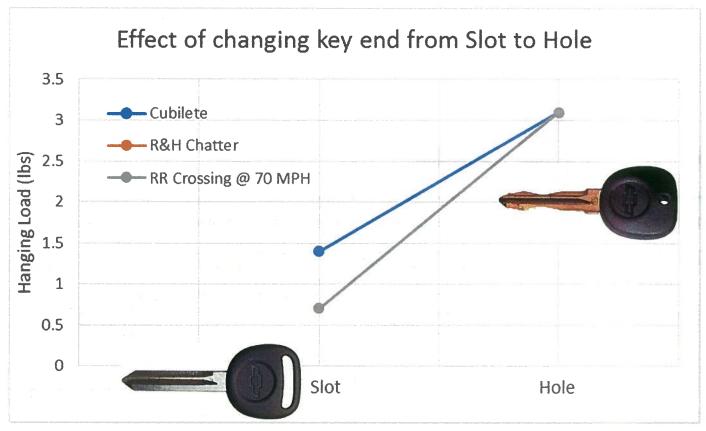


# Effect of Switch Torque

Vehicle	Cobalt				
Key	Slot				
Switch		8.4 N*cm	12.9 N*cm	20.3 N*cm	
Ride and Handling loop @ posted speeds	nass with rotation ds)	0.7	1.0	2.4	
Belgian Blocks durability schedule		0.8	1.2	2.2	
Pothole #1 @25 MPH		0.7	1.2	1.7	
Pothole #2 @ 25 MPH	mass d rota nds)	0.9	1.3	2.4	
Cubilete @ 10 MPH	num mass ended rot (pounds)	0.8	1.4	2.4	
Panic stop from 10 mph	imi iter (F	1.0	1.9	3.0	
R&H Chatter @ 45 - 55MPH Hz=MPH/3	Minimum m unintended (poun	0.6	0.7	2.2	
R&H Angled RR crossing @ 70 mph		0.6	0.7	1.0	



# Test Results – Original Design



Plotted the minimum load for each test signal that ended with ignition switch in 'accessory' position with a 12.9N\*cm switch.

Conditions with hole never experienced unintended rotation, and testing was stopped @ 3.1#



## Effect of Hole vs. Slot

Vehicle	Cobalt				
Switch	12.9 N*cm		12.9 N*cm		
Key	Slot		Hole*		
Cubilete @ 10 MPH	Minimum mass	1.4	Max mass tested,	3.1	
R&H Chatter @ 45 - 55MPH Hz=MPH/3	where rotation	0.7	rotation did not	3.1	
R&H Angled RR crossing @ 70 mph	occurred. (pounds)	0.7	occur. (pounds)	3.1	

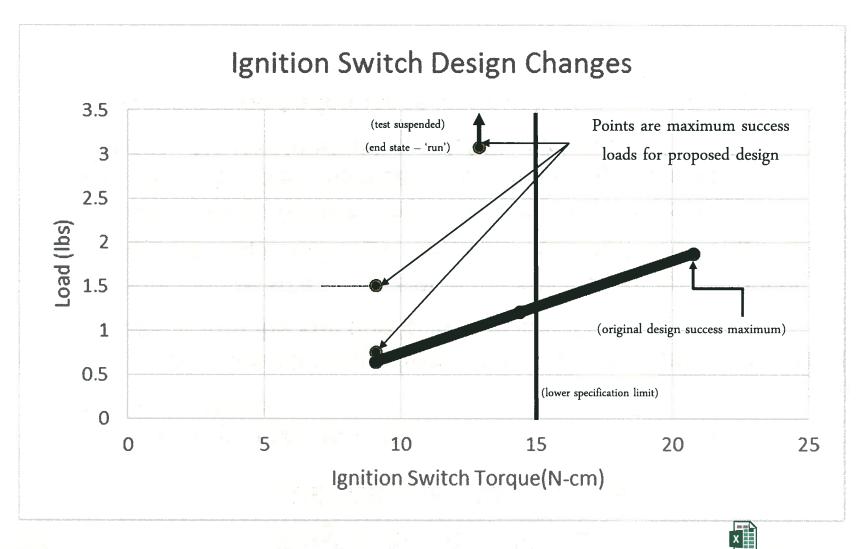
<sup>\*</sup>Configurations with hole & 13mm ring never experienced unintended rotation. Testing stopped at 3.1#







# Test Results – Proposed Design







# **Key Concept Phase Learnings/Decisions**

- Original design used to establish drive schedules and key ring loading transition
  - Increasing switch torque from run to acc increases the required mass to turn the key due to inertial loading.
  - -Reducing the size of the slot in the key (to a hole) increases the mass required to turn the key due to inertial loadings.
- Proposed design (switch torque 20 N\*cm + / 5 N\*cm, and change key to hole) assessed using drive schedules and key loadings. No unintended key rotation occurred.
- Proposed design performance improved from original design



# Backup



## **Physics**

Ring weight = 0.031 Newtons (0.007lb)

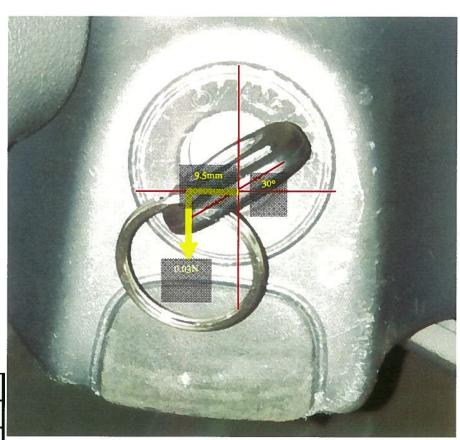
Slot length in key head = 2.2 cm

Moment arm = 1/2 slot length \* cos theta = 0.95 cm

Static Moment = 0.031 N \* 0.95cm = 0.03 N\*cm

Input moment due to inertial forces is negligible with key and ring only.

"g" level	N*cm of torque generated
33	1
67	2
133	4
267	8
533	16





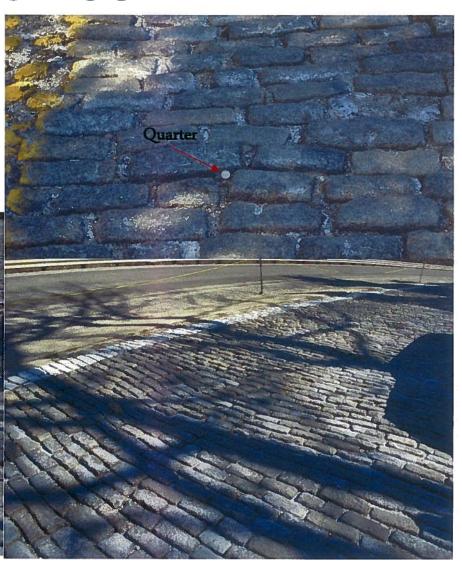
## Road system images

- Road test descriptions:
  - -Belgian Blocks durability schedule
  - -Pothole #1 @25 MPH
  - -Pothole #2 @ 25 MPH
  - -Cubilete @ 10 MPH
  - -Panic stop from 10 mph self explanatory
  - -Ride and Handling loop @ posted speeds
  - -R&H Chatter @ 45 55MPH Hz=MPH/3
  - -R&H Angled RR crossing @ 70 mph
  - -Median crossing from 15 50 MPH
  - -Median crossing w/ braking from 35 45 MPH

# Belgian Blocks 25 - 35MPH

• A 1.7 mile replica of old Belgian granite block roads that are very rough, including dips and bumps to accelerate durability.



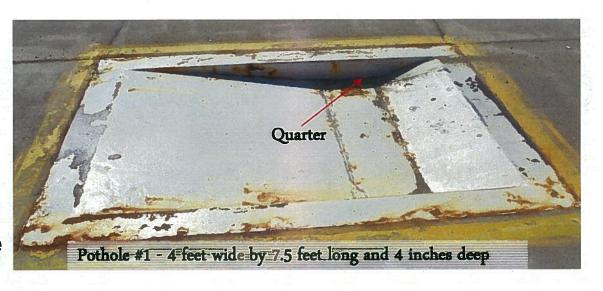


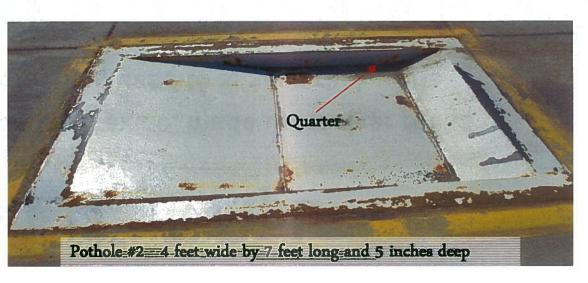
# DFSS

# Potholes #1 & #2 @ 25 mph

- Pothole #1 a 50<sup>th</sup>
   percentile customer would
   see at least one of these
   vertical load events in a the
   vehicle's life.
- Pothole #2 a 80<sup>th</sup> percentile customer









## La Cubilete @ 10 mph

A replica of a severe road in Mexico, made up of river rocks

Not part of standard durability, used to assess rack rattle





# Chatter Bumps from 55 - 45 MPH - A series of evenly spaced bumps that excite suspension motion. Frequency ==mph /3

## Ride and Handling Loop

Ride & Handling Angled RR crossing @ 70 MPH - An elevated, railroad crossing that is at an angle to the road direction





# **Physics**

Significantly reduced moment arm



